



Heat transfer Convection

I.Forced convection-continued

1. Correlations for flows around a cylinder

We choose the simplest correlation: $2 \ 10^4 < \text{Re} < 4 \ 10^5 \text{ et Pr} > 0.2$:

$$Nu_D = 0.3 + \frac{0.62Re_D^{0.5} Pr^{0.33}}{\left[1 + \left(\frac{0.4}{Pr}\right)^{0.67}\right]^{0.25}} \left[1 + \left(\frac{Re_D}{282000}\right)^{0.5}\right]$$
(1)

- Case of liquid metals

$$Nu_D = \left[0,8237 - \ln\left(Pe_D^{0,5}\right)\right]^{-1}$$
⁽²⁾

2.Correlations for flows around a sphere

0.71 < Pr < 380 and $3.5 < Re < 7.6 \ 10^{4}$. The following correlation is applicable:

$$Nu_D = 2 + (0.4Re^{0.5} + 0.06Re^{0.67})Pr^{0.4} \left(\frac{\mu}{\mu_{\infty}}\right)^{0.25}$$
(3)

3. Correlations for internal flows in tubes

a) Laminar regime

The laminar regime in the tubes is determined by Re < 2300.

In the case of circular tubes with uniform surface in laminar regime at constant flow, the Nusselt number is constant:

 $Nu_D = 4.36.$

In the case of circular tubes with constant surface temperature, the Nusselt number is also constant:

 $Nu_D = 3.66.$

b) Turbulent regime

The most used correlation for smooth tubes is the following:

 $Nu = 0.023 Re 0.8 Pr^n$

(4)

With: n = 0.3 for cooling and n = 0.4 for heating.





II.Correlations for natural convection

In natural convection, we use the numbers of Pr and Gr therefore (Ra = Pr x Gr).

All correlations have the following form:

 $Nu = C (Gr xPr)^n = Cx Ra^n$ (5)

C and n depend on the geometry of the surfaces.

1.Vertical plates

$$\overline{Nu_L} = 0,59 \times Ra_L^{0.25} \qquad 10^4 \le Ra_L \le 10^9$$

$$\overline{Nu_L} = 0,10 \times Ra_L^{0.33} \qquad 10^9 \le Ra_L \le 10^{13}$$
(6)
(7)

A more general correlation can also be applied in all these cases regardless of the Raleigh number:

$$\overline{Nu}_{L} = \left\{ 0,825 + \frac{0,387 Ra_{L}^{0,16}}{\left[1 + (0,492/Pr)^{0.56} \right]^{0.3}} \right\}^{2}$$
(8)