

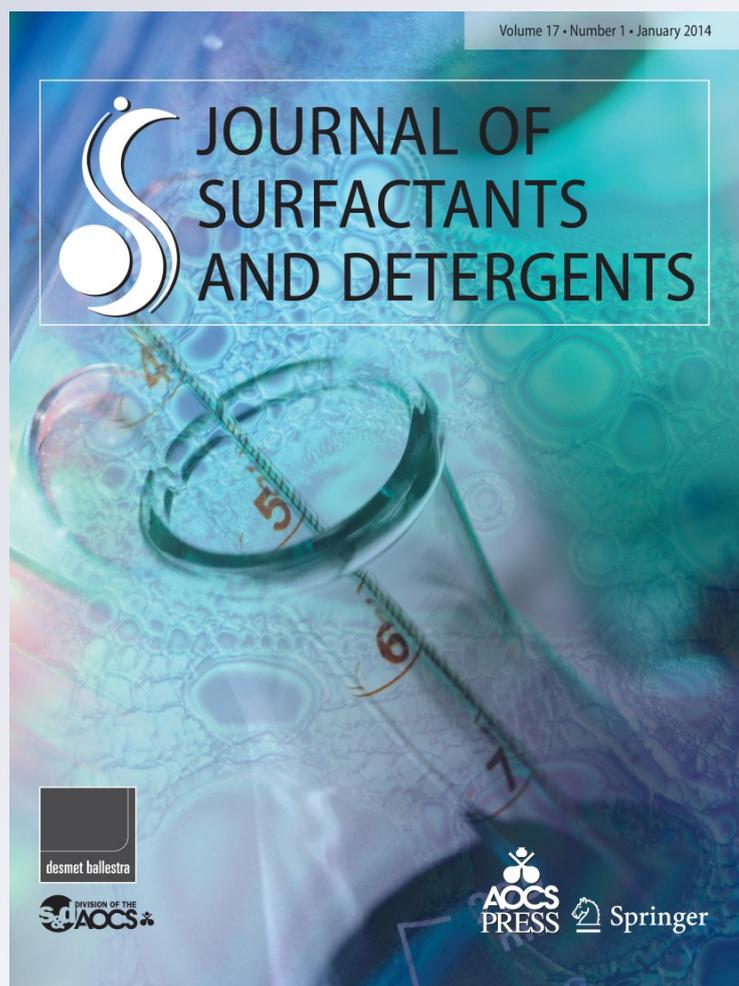
*Removal of Copper(II) from a Concentrated Sulphate Medium by Cloud Point Extraction Using an N,N#-Bis(salicylaldehyde)Ethylenediimine Di-Schiff Base Chelating Ligand*

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# Removal of Copper(II) from a Concentrated Sulphate Medium by Cloud Point Extraction Using an *N,N'*-Bis(salicylaldehyde)Ethylenediimine Di-Schiff Base Chelating Ligand

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**Abstract** Various chelating ligands have been investigated for the cloud point extraction of several metal ions. However, limited studies on the use of the Schiff base ligands have been reported. In this work, cloud point extraction behavior of copper(II) with *N,N'*-bis(salicylaldehyde)Ethylenediimine Schiff base chelating ligand, ( $H_2SALEN$ ), was investigated in aqueous concentrated sulphate medium. The extraction process used is based on the formation of hydrophobic  $H_2SALEN$ –copper(II) complexes that are solubilized in the micellar phase of a non-ionic surfactant, i.e. ethoxylated (9.5EO) *tert*-butylphenol. The copper(II) complexes are then extracted into the surfactant-rich phase above cloud point temperature. Different parameters affecting the extraction process of Cu(II), such as equilibrium pH, extractant concentration, and non-ionic surfactant concentration were explored. The extraction of Cu(II) was studied in the pH range of 2–11. The results obtained showed that it was profoundly influenced by the pH of the aqueous medium. The concentration factor,  $C_f$ , of about 17 with extraction efficiency of  $E\% \approx 100$  was achieved. The stoichiometry of the extracted complex of copper(II) was ascertained by the Yoe–Jones method to give a composition of 1:1 (Cu: $H_2L$ ). The optimum conditions of the extraction-removal have been established as the following: (1)  $1.86 \times 10^{-3}$  mol/L ligand; (2) 3 wt% surfactant; (3) pH of 8 (4) 0.5 mol/L  $Na_2SO_4$  and (5) temperature of 60 °C.

**Keywords** Cloud point extraction · Copper(II) · Schiff base chelating ligand · Sulphate media · *N,N'*-bis(salicylaldehyde)Ethylenediimine · Alkyl phenol ethoxylate

## Introduction

Solvent extraction is one of the most effective separation processes, and is widely used for the separation and recovery of several heavy metal ions [1]. However, this technique has some restrictions and presents drawbacks due to the use of expensive, hazardous and flammable organic solvents. An interesting alternative to traditional solvent extraction is cloud point extraction (CPE), initially developed by Watanabe and co-workers [2].

The process of cloud point extraction is based on the property that an aqueous solution of non-ionic surfactant forms micelles and becomes turbid when heated to a temperature known as the cloud point temperature (CPT). Above this temperature, the micellar solution separates in a surfactant-rich phase of a small volume and diluted aqueous phase, in which the surfactant concentration is close to the critical micellar concentration (CMC). Accordingly, any component originally present in the solution that interacts with surfactant aggregates (micelles) either directly or after chelation by hydrophobic extractant can thus be separated and concentrated in the small surfactant-rich phase [3–6].

The cloud point temperature of the non-ionic surfactant can be affected by many factors such as its own concentration and the number of ethylene oxide units in its molecules as well as additives like electrolytes [7–11].

As novel separation process, CPE offers many advantages over traditional solvent extraction. Indeed, this process uses water and reduces the consumption of and

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ethanol. On the other hand, it has two nitrogen atoms and hydroxyl groups in complexation with copper.

### Instrumentation

A Shimadzu 1202 model UV–Visible spectrophotometer with 10-mm quartz cells was used for the determination of the concentration of metal. The pH values were measured with an accuracy of 0.02 pH units, using a Schott-Geräte model CG820 pH-meter, equipped with a glass-combination electrode. A thermostated bath maintained at the desired temperatures was employed for cloud point experiments.

### General Procedures

#### Cloud Point Determination

The temperature at which the cloud point phenomenon occurs was determined by the method reported by Carvalho et al. [41]. The method is based on the visual observation of the separation of phases in the micellar solution. The initial aqueous solution (25 mL) was heated in a thermostated vessel at a specific temperature which was well above its cloud point (turbid solution). Then the solution was cooled gradually. The cloud point was considered as the temperature at which the solution became clear. To verify the results, the opposite process was carried out by gradually heating the clear solution until turbidity appeared. The reported value was the average of these two determinations. In most cases, these two temperatures were identical, within 0.5 °C.

#### Typical Cloud- Point Extraction

First, 25 mL of the analytical solution mixture containing  $1.57 \times 10^{-3}$  mol/L Cu(II),  $1.86 \times 10^{-3}$  mol/L Schiff base, 3 wt% TOP9.5EO, and 0.5 mol/L of Na<sub>2</sub>SO<sub>4</sub> was adjusted to the appropriate pH value (pH = 8) with NaOH. Then, the system was stirred for 5 min in a shaker and transferred to a 10-mL test tube with a graduated line. After that, the test tube was kept in a constant temperature bath for 6 h at 60 °C. The copper concentration was determined spectrophotometrically in the dilute aqueous phase. The volume of the surfactant-rich phase was registered to an accuracy within  $\pm 0.1$  mL units.

## Results and Discussion

### Calculations

The distribution coefficient parameter used to describe the degree of metal partitioning from the aqueous to the surfactant-rich phase, is given by:

$$D_M = \frac{[M]_s}{[M]_w} \quad (1)$$

where  $[M]_s$  and  $[M]_w$  are the final metal concentrations in the surfactant-rich phase and in the aqueous phase, respectively.

The efficiency of process,  $E$  %, can be expressed as:

$$E = 100 \frac{D_M}{D_M + \frac{V_w}{V_s}} \quad (2)$$

where, the  $V_w$  and  $V_s$  refer the volumes of dilute aqueous solution and surfactant-rich phase obtained after the extraction step, respectively.

Finally, the concentration factor and the volume fraction of the surfactant-rich phase are given by:

$$C_f = \frac{E}{100 \varphi_s} \quad (3)$$

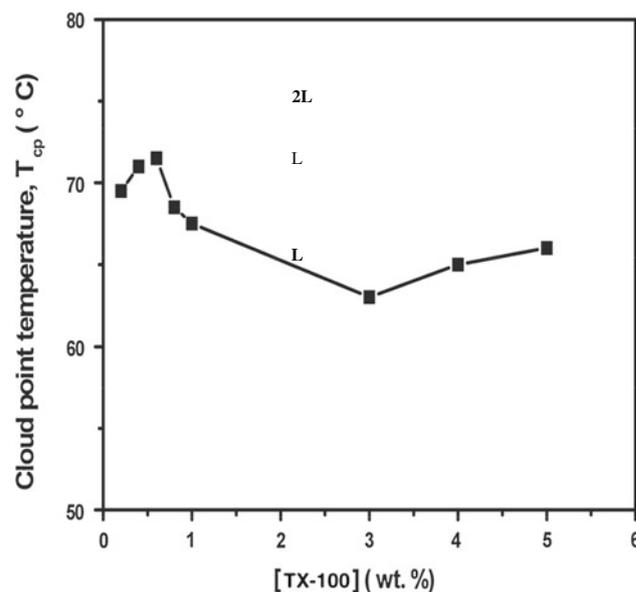
$$\varphi_s = \frac{V_s}{V_0} \quad (4)$$

where  $V_0$  is the volume of the original aqueous solution prior to the extraction step.

### Phase Diagrams of Binary Systems

#### Characterization of the Phase Diagram of a Triton X-100 Water System

The phase diagram of the non-ionic surfactant TOP9.5EO obtained in this study at different aqueous concentrations, ranging from 0.1 to 5 wt% is shown in Fig. 2. The shape of



**Fig. 2** Phase diagram of a TOP9.5EO—water—binary system. *L* one phase, *2L* two phases

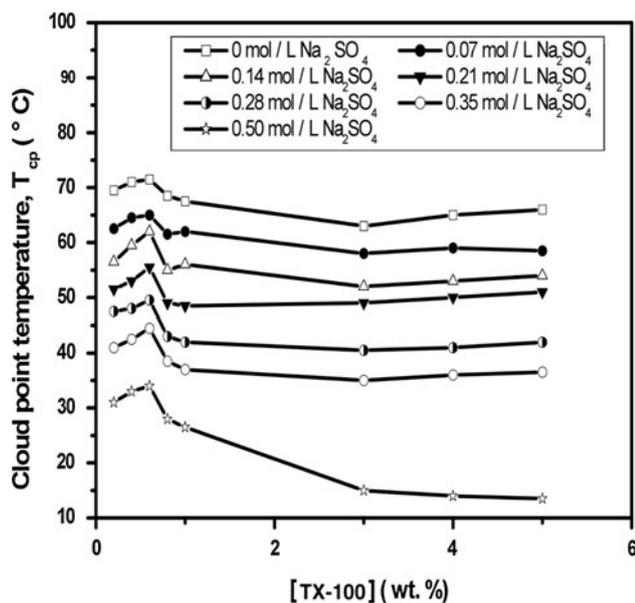
the curve coincides with that expected for a typical non-ionic surfactant [42]. Below the curves, there are micellar solutions (1L), while two-phase regions co-exist above the curves (2L).

It has been mentioned by several authors that solutions of non-ionic surfactants generally can show different critical temperatures at similar concentrations depending upon the experimental conditions and purity of the amphiphiles [4]. Non-ionic polyoxyethylene surfactants are usually synthesized as a mixture of oligomers characterized by an average number of oxyethylene units. Furthermore, the presence or addition of other compounds to the amphiphile solution can lead to change in the clouding process. Thus, one should not expect complete agreement among the results obtained by different researchers unless the experiments have been carefully controlled and all operating conditions are exactly repeated.

As evident from the phase diagram given in Fig. 3, the lowest cloud point temperature ( $T_{cp}$ ) value determined for TOP9.5EO was 63 °C at a concentration of 3 wt%. Moreover, the cloud point temperature,  $T_{cp} = 67$  °C, found at the surfactant concentration of 1 wt% was in good agreement with that reported by Mata [43], for a micellar solution of TritonX-100 without any additives.

#### Effect of Sodium Sulphate

The influence of adding  $\text{Na}_2\text{SO}_4$  (0–0.5 mol/L) on the cloud point temperatures of the TOP9.5EO micellar solutions was examined at various surfactant concentrations. Figure 3 clearly demonstrates that the addition of sodium sulphate lowers the cloud point curve. This phenomenon



**Fig. 3** Phase diagram of TOP9.5EO—water— $\text{Na}_2\text{SO}_4$  ternary systems

can be conveniently explained in terms of an earlier dehydration of the ethoxylated chains due to the presence of inorganic ions (sodium sulphate in this case:  $\text{Na}^+$  and  $\text{SO}_4^{2-}$ ) competing for the interaction with the water molecules, i.e. a “salting-out” effect.

Also, it seems that sodium sulphate lowers the cloud point by a continuous medium change, more than by direct interaction with the ethoxy groups of the surfactant [42, 44–46].

Figure 3 shows how 0.5 mol/L of  $\text{Na}_2\text{SO}_4$  is able to lower the cloud point of a 3 wt% Triton X-100 solution from 63 to 15 °C. Therefore, it is possible to adjust the cloud point to room temperature and facilitate the cloud point extraction process by simply controlling surfactant and salt concentrations. Salt addition can also increase the density of the dilute phase; this makes the separation of both dilute and surfactant rich phases easy in some non-ionic surfactant systems [2, 47].

#### Equilibrium Distribution Coefficients of Copper(II)

The cloud point extraction process of copper(II) by  $N,N'$ -bis(salicylaldehyde)Ethylendiimine dissolved in TOP9.5EO nonionic surfactant micellar solutions was investigated over a pH range of approximately 2–11. The concentrations of the ligand and TOP9.5EO were between  $10^{-4}$  mol/L and  $5 \times 10^{-3}$  mol/L, and 0.8 and 5 wt%, respectively. The results of the equilibrium distribution coefficients,  $D_M$  of copper(II) between the dilute aqueous phase and surfactant-rich phase are presented in Tables 1, 2, 3. As shown in Table 1, it can be seen that the distribution coefficients of Cu(II) are higher in the basic pH

**Table 1** Influence of equilibrium pH on distribution coefficient,  $D_M$  and extraction efficiency,  $E$  % of copper(II)

Equilibrium pH	$D_M$	$E$ %
2.58	3	17
3.37	4	21
4.16	5	25.5
5.02	6	29
6.25	14	47
6.60	22	58
7.03	ND	100
7.53	ND	100
7.81	ND	100
8.02	ND	100
9.29	60	79
11.04	54	77

$[\text{Cu}^{2+}] = 1.57 \times 10^{-3}$  mol/L,  $[\text{H}_2\text{L}] = 1.86 \times 10^{-3}$  mol/L,  $[\text{Na}_2\text{SO}_4] = 0.5$  mol/L,  $[\text{TOP9.5EO}] = 3$  wt%,  $T = 60$  °C,  $\varphi_s = 0.06$

ND Not determined because of high extractability

range. Because *N,N'*-bis(salicylaldehyde)Ethylenediimine Schiff base is a basic extracting agent, copper(II), which is a common Lewis acidic metallic ion, was easily extracted from aqueous sulphate solutions by complex formation. Moreover, the distribution coefficient increased with an increase in pH. This confirms that the CPE process has taken place via a cation exchange mechanism. On the other hand, it is obvious from the data indicated in Tables 2 and 3 that the distribution coefficients of Cu(II) initially increase, and then decrease as the ligand and surfactant concentrations are increased. The increase in  $D_M$  is presumably due to the increase in the complex concentration and solubilization power of the non-ionic surfactant TOP9.5EO micelles. A similar conclusion has been reported by Favre-Réguillon et al. [48] for the cloud point extraction of lanthanides(III) by 8-hydroxyquinoline.

### Optimization of the CPE Process

The efficiency of the cloud point extraction process of metals depends on a number of parameters, namely concentration of the extractant, concentration of the surfactant and solution pH. In the present study, these parameters were investigated in order to find the optimal operation conditions.

### Effect of Solution pH

For ionisable solutes, the charge of the solute can greatly influence its extent of binding to a micellar assembly [49]. The ionic form of a molecule normally does not interact with and bind the micellar aggregate as strongly as does its neutral form. Indeed, adjustment of the micellar solution pH is the key-parameter when controlling experimental variables in the cloud point extraction process.

An interesting result was obtained in the study of the influence of solution pH on the extraction recovery of the studied cations. In this series of experiments, the solution pH was varied over the range of 2–11. The Triton X-100, *N,N'*-bis(salicylaldehyde)Ethylenediimine, copper, and  $\text{Na}_2\text{SO}_4$  concentrations were kept constant at 3 wt%,  $1.86 \times 10^{-3}$  mol/L,  $1.57 \times 10^{-3}$  mol/L, and 0.5 mol/L, respectively. The experiments were carried out at a separation temperature of 60 °C. Table 1 shows the effect of pH on the extraction efficiencies of Cu(II) complexes. It can be seen that extraction was quantitative for copper(II) in the pH range 7–8. At lower pH values, the formation of complexes is not quantitative, and at higher pH values, the extraction starts to decrease. A similar pattern of the pH effect has been reported in the literature for the extraction of copper with different ligands such as 1-(2-pyridylazo)-2-naphthol (PAN), isoleucine and pyrogallol [50–52].

Therefore, based on these findings, an optimised pH of 8 was selected for the CPE system.

### Effect of Chelating Ligand Concentration

In order to achieve the total extraction and preconcentration of copper(II), a series of experiments was carried out in which the other experimental variables, except extractant concentration, remained constant. Table 2 highlights the differences in the efficiencies at different extractant concentrations over the range of  $10^{-4}$  to  $5 \times 10^{-3}$  mol/L. It is shown that the efficiencies ( $E$  %) of the extraction of copper increase with the concentration of the chelating extractant, *N,N'*-bis(salicylaldehyde)Ethylenediimine ( $\text{H}_2\text{SALLEN}$ ). An extractant concentration of  $1.86 \times 10^{-3}$  mol/L permitted us to achieve the total formation of the complex and about 100 % extraction efficiency. On the other hand, when an excess of extractant was used ( $3 \times 10^{-3}$  mol/L), a decrease in the efficiency was observed (94 %). This behaviour can be explained because the molecules of

**Table 2** Influence of initial concentration of extractant on the distribution coefficient,  $D_M$  and extraction efficiency,  $E$  % of copper(II)

$[\text{H}_2\text{L}]/\text{mol/L}$	$D_M$	$E$ %
$10^{-4}$	4	21
$2 \times 10^{-4}$	5	25
$3 \times 10^{-4}$	12	44
$5 \times 10^{-4}$	16	51
$1.41 \times 10^{-3}$	208	93
$1.86 \times 10^{-3}$	ND	100
$3 \times 10^{-3}$	245.5	94
$4 \times 10^{-3}$	232	94
$5 \times 10^{-3}$	193	92.5

$[\text{Cu}^{2+}] = 1.57 \times 10^{-3}$  mol/L,  $[\text{Na}_2\text{SO}_4] = 0.5$  mol/L,  $[\text{TOP9.5EO}] = 3$  wt%, pH = 8,  $T = 60$  °C,  $\varphi_s = 0.06$

ND Not determined because of high extractability

**Table 3** Influence of initial concentration of surfactant on the distribution coefficient,  $D_M$  and extraction efficiency,  $E$  % of copper(II)

TOP9.5EO/wt%	$D_M$	$E$ %
0.8	55	53
1	206	86
2	497	95
3	ND	100
4	40	75
5	27	73

$[\text{Cu}^{2+}] = 1.57 \times 10^{-3}$  mol/L,  $[\text{H}_2\text{L}] = 1.86 \times 10^{-3}$  mol/L,  $[\text{Na}_2\text{SO}_4] = 0.5$  mol/L, pH = 8,  $T = 60$  °C

ND Not determined because of high extractability

extractant are presumably trapped in the micelles, thus reducing the concentration of the complex. Finally, it should be pointed out that similar results were mentioned in other published studies concerning the cloud point extraction of copper and chromium with analogous Schiff base chelating ligands [36, 53].

#### Effect of Surfactant Concentration

The concentration of surfactant that is used in CPE is a critical parameter. A successful cloud point extraction would be that which maximizes the efficiency of extraction through minimizing the phase volume ratio, and thus maximizing its concentrating factor. To obtain the optimal concentration of TOP9.5EO, the effect of surfactant concentration on the extraction efficiency of the system was investigated over the range of 1–5 wt%. The results are shown in Table 3. A concentration of 3 wt% was selected as the optimum concentration for the extraction of copper. At concentrations below this value, the efficiency of the extraction of the complexes and efficiency of the process were low because there are few molecules of the surfactant to entrap the complex quantitatively. At concentrations higher than 3 wt% of TOP9.5EO, the efficiencies decrease because of the volume and viscosity increases of the surfactant phase. These results are in qualitative agreement with other literature reports investigating the effects of increases in surfactant concentration upon the extraction efficiency of several metal ions [18, 22, 26, 36, 53].

#### Concentration Factor, $C_f$ and Phase Volume Fraction, $\phi_s$

Performance of a CPE process can be also assessed by its surfactant rich-phase volume fraction,  $\phi_s$  and concentration factor,  $C_f$ . These two parameters are defined in the.

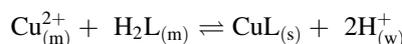
“Calculations” Table 4 reflects the variation of  $\phi_s$ ,  $C_f$ , and extraction efficiency,  $E$  %, of copper(II) of the TOP9.5EO/ $\text{Na}_2\text{SO}_4$ / $\text{H}_2\text{SALEN}$  CPE process with respect to the concentration of the non-ionic surfactant. At a fixed sample volume,  $C_f$  initially increases and then decreases as the concentration of the non-ionic surfactant increases.

In general, with less surfactant in the solution, the volume of the surfactant-rich phase thus formed becomes smaller and, hence, the concentration of the extracted analyte in the surfactant-rich phase increases. However, further reduction in the surfactant concentration will eventually lead to insufficient surfactant in the surfactant-rich phase to efficiently extract the analyte, causing a drop in analyte extraction. From Table 4, it is seen that a concentration of non-ionic surfactant of 1 wt% provides a high concentration factor ( $C_f = 29$ ) and extraction efficiency ( $E$  %  $\approx 86$  %) with an acceptable surfactant-rich phase

volume fraction of  $\phi_s = 0.03$  ( $0.02 \leq \phi_s \leq 0.1$ ) [54]. On the other hand, the results show that the volume fraction ( $\phi_s$ ) of the surfactant increases with increasing concentration of TOP9.5EO. Similar behaviour was observed in other CPE processes using non-ionic and ionic surfactants [12, 55, 56].

#### Stoichiometry of the Extracted Complexes

The mole ratio method, resulting in the so-called Yoe–Jones [57] plots, was used to determine the stoichiometry of the complex Cu(II)- $\text{H}_2\text{SALEN}$  formed. The Yoe–Jones method was performed by heating a series of mixtures of solutions of copper sulphate and extractant at 60 °C for 6 h at pH = 8. The extractant concentration ( $\text{H}_2\text{L}$ ) was varied from ( $10^{-4}$  to  $5 \times 10^{-3}$ ) mol/L with a constant copper(II) concentration ( $1.57 \times 10^{-3}$  mol/L). The mole ratio plot showed only one break, corresponding to the formation of a 1:1 complex between copper ion and  $\text{H}_2\text{L}$  (Fig. 4). From this result and taking into account that the extraction of Cu(II) proceeds via a cation exchange mechanism in the pH range 7–8, the extraction process may be represented by the following equation:



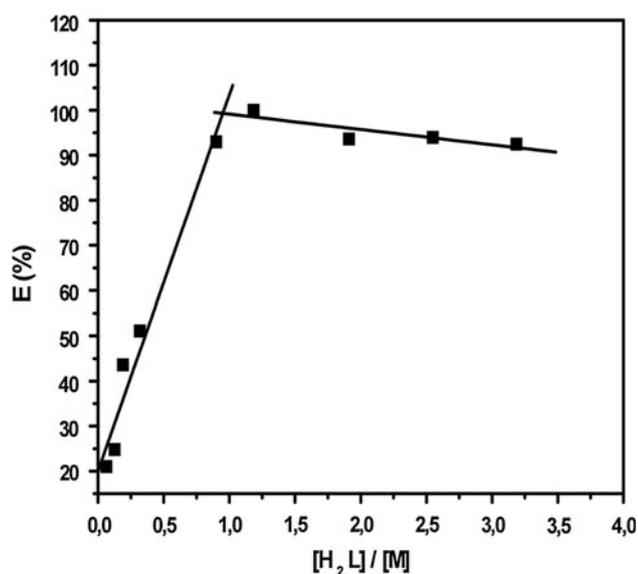
[(m) denotes the species in the homogeneous micellar solution; (w) and (s) refer to the species in the aqueous and surfactant-rich phases, respectively].

#### Comparison of Performance of the Present Chelating Ligand with Others for CPE of Copper(II)

For comparison purposes, the extraction efficiency ( $E$  %), the separation temperature ( $T_s$ ) and the concentration factor ( $C_f$ ) of the cloud point extraction of copper(II) by the proposed chelating ligand and those previously reported ligands are given in Table 5 [50, 51, 58–62]. As can be seen, the extraction efficiency ( $E$  %) and the concentration factor ( $C_f$ ) of the present chelating ligand in

**Table 4** Effect of the surfactant concentration on the concentration factor ( $C_f$ ) and the surfactant-rich phase volume fraction ( $\phi_s$ ) of the CPE process performance:  $[\text{H}_2\text{L}] = 1.86 \times 10^{-3}$  mol/L,  $[\text{Na}_2\text{SO}_4] = 0.5$  mol/L, pH = 8,  $T = 60$  °C

TOP9.5EO/wt%	$E$ %	$C_f$	$\phi_s$
0.8	53	26.5	0.02
1	86	29	0.03
2	95	24	0.04
3	100	17	0.06
4	75	11	0.07
5	73	8	0.09



**Fig. 4** Determination of the stoichiometry of the extracted copper(II)-H<sub>2</sub>SALEN complex by the mole ratio method. [Cu<sup>2+</sup>] = 1.57 × 10<sup>-3</sup> mol/L; pH = 8; [Na<sub>2</sub>SO<sub>4</sub>] = 0.5 mol/L; T = 60 °C ⇌

this work are superior to those of most other reported ligands. Besides, under the same experimental conditions, it seems that the system H<sub>2</sub>SALEN/Triton X-100 exhibits a higher concentration factor and a lower separation temperature ( $C_f = 29$ ,  $T_s = 60$  °C) than the system H<sub>2</sub>SALDIEN/TOP9.5EO ( $C_f = 14$ ,  $T_s = 65$  °C), reported in our previous study [53]. On the other hand, the separation, temperature ( $T_s$ ) of the extraction process is comparable with, and in some cases lower than the reported ones [50, 51, 59, 62]. Finally, it should be emphasized that chemical structure and cloud point temperature of the non-ionic surfactant employed for extraction can seriously alter the separation temperature of the cloud point extraction of metals [63, 64].

## Conclusions

In this study, the combined advantages of the cloud-point extraction process and the use of polydentate Schiff base *N,N'*-bis(salicylaldehyde)Ethylenediimine as a chelating ligand were utilized for the extraction of copper(II) in an aqueous sulphate medium. From the results obtained, the following conclusions can be drawn: (1) The cloud point extraction is an easy, practical and a very promising process for the extraction and separation of copper(II). It offers an inexpensive and non-polluting alternative to other separation extraction processes. (2) *N,N'*-bis(salicylaldehyde)Ethylenediimine proved to be an efficient chelating ligand for quantitative cloud point extraction of copper(II). The simple synthesis, the formation of stable complexes and consistency with the cloud point extraction process are the major advantages of the use of this type of ligand in cloud point extraction of copper. (3) The extent extraction is markedly influenced by the pH of the aqueous solution, the concentration of the extractant and non-ionic surfactant. (4) The optimized experimental parameters for quantitative extraction ( $E \% \approx 100$  %) are: (1)  $1.86 \times 10^{-3}$  mol/L of ligand; (2) 3 wt% surfactant; (3) pH of 8 and (4) temperature of 60 °C. (5) The environmental pollution is limited to a small amount of surfactant. This fact is particularly attractive because the “green chemistry” concept can be employed here.

Although the suggested CPE system offers a good extraction ability for copper(II), much more work is obviously needed to fully understand the CPE process. This includes the following: (1) Elucidation of the nature of the interaction and binding between the extracted species with this kind of extractant and the non-ionic surfactant micelles; (2) separation of copper ions from copper complex-entrapped surfactant and, hence, the regeneration of the extractant by the application of the pH-switching

**Table 5** Comparison of the performance of the present chelating ligand with others for the CPE of copper(II)

Ligand	Surfactant	E %	$C_f$	$T_s$	References
Monocarboxylic aromatic acids	OP-10	30–90	ND	75	[58]
MPKO	TOP7.5EO	100	30	45	[59]
1-PTSC	TOP7.5EO	97	25	50	[60]
Alizarin red	TOP7.5EO	96	21	70	[61]
Isoleucine	TOP9.5EO	96	22	65	[51]
Me-BDBD	TOP7.5EO	95	14	45	[62]
PAN	TOP7.5EO	96	16	50	[50]
H <sub>2</sub> SALDIEN	TOP9.5EO	100	14	65	[53]
H <sub>2</sub> SALEN	TOP9.5EO	100	29	60	This work

ND Not determined, MPKO methyl-2-pyridylketone oxime, 1-PTSC 1-Phenylthiosemicarbazide, Me-BDBD 6-[2-(6-methyl-benzothiazolylazo)]-1,2-dihydroxy-3,5-benzenedisulfonic acid, PAN 1-(2-pyridylazo)-2-naphthol (PAN), H<sub>2</sub>SALDIEN *N,N'*-bis(salicylideneaminoethyl)amine, H<sub>2</sub>SALEN *N,N'*-bis(salicylidene)Ethylenediimine

process; (3) increase the selectivity of the CPE process with this type of polydentate Schiff base extractant in order to accomplish extraction of copper from a multimetal solution.

Finally, further work is under way in our laboratory to generalize the cloud point extraction technique with this type of polydentate Schiff base ligand for the separation-removal of other heavy metals such as Ni(II), Cd(II) or Pb(II).

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